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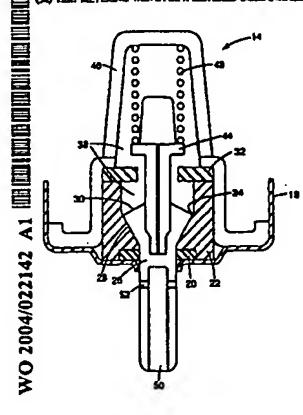
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(54) TIDIN METERDASI VALVE FOR A METERED DOSE D'HALER PROVIDESS CONSISTENT DELIVERY



(57) Abstract: The present invention relates to a sever dadge for a metalog value that provides improved con-sistency of formulation delivery. Generally, the meaning raive includes (a) a valve etem that generally defines a lowgiradiest axis and includes a body parties having a metering earthes, wherein the bregistational asts and a prison mo ded to at least a practice of the controlling sections define na angle from about 2" to about 90"; and (b) a value body haring an intermal chamber defined at least in past by the body well and includes a marriag portion configured to ationly conform to the metaring curtices of the valve

PCT/US2003/027587 WO 200UR22142

METERING VALVE FOR A METERED DOSE INHALER PROVIDING CONSISTENT DELIVERY

Background

Metaring valves are a common means by which acrosols are dispersed from acrosol containers. Metering valves are particularly useful for administrating medicinal formulations that include a liquefled gas propellent and are delivered to a patient in an acrosol.

When administrating medicinal formulations, a close of formulation sufficient to 10 produce the desired physiological response is delivered to the patient. The process productionized emount of the formulation must be dispersed to the perions in each anccessive does. Thus, any dispensing system usest be able to dispense doses of the medicinal framulation accurately and reliably to belt assum the sufety and efficacy of the trestment.

Metering valves have been developed to provide control over the dispensing of medicinal acrossi formulations. A metering valve may be used to regulate the volume of a medicinal formulation pessing from a container to a metering chamber, which defines the maximum amount of the formulation that will be dispersed as the next does. Reliable and controllable flow of the medicinal framulation into the metraling chamber may contribute to the accounty and/or practicion of the matering of accountive doses of the freembation. Thus, reliable and exemplable flow of the medicinal formulation into the metering chamber may improve performance of the metaring valve and, therefore, may be highly desirable.

In some metering valves, the metering chamber fills with the medicinal formulation prior to the periors actuating the valve stem and thereby releasing the dese. The meaning cisember is refilled with the metaring only dispersing one does no that the metaring vulve is ready to discharge the next dose. Consequently, the metering chamber contains formulation at all times except for the brief time during which the valve store is depressed by the ener to discharge a close. Also, the passageways through which the firemphotics ment flow to reach the metering chumber are often pursue and tortuces. As a result, metading values configured to this way have a market of disadvantages resulting in, for

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PCT/US2063/027587 WO 2004022142

example, caratic doming due to loss of prime. "Loss of prime" means the occurrence of vapor or air voids in the metered volume, thereby leading to a shortfull in the volume of dose being metered by the valve. A principal cause of less of prime is the presence of cratifications in the entry passageway or passageways through which themshiften must pass to fill the metering chember. Such restrictions can lead to flow disruption and than also to the occurrence of vapor or air voids in the metering chamber.

Another phenomenon that can lead to erratic during is less of doze. "Loss of doze" means a change in the amount of suspended thing or excipient particles in a metered dose of formulation, compared to the average composition of the balk formulation in the container. A principal cause of loss of dose is the senting of dong particles into, or their movement out of, restricted regions of the metaring valve such that the proper concentration of farmphring cannot subsequently be obtained within the married regions prior to does delivery. For example, drug particles may settle in a residual metering volume - any part of the metering valve bounded by a metering number and that, when the metering valve is in the resting position, recuring fluid filled but is not in substantially freeflowing communication with the balk formulation.

In other metering valves, residual metering volume may be limited to some extent by designing the metering valve so that the metering chamber does not materialize unless and such the valve stem is actuated. However, even in these metering valves, a small residual metaring volume exists when the metaring valve is at cest because a small emotion gap exists between the valve stem and the metering valve body.

Actuation of these valve stems can be divided into a filling steps and a discharge stage. The filling stage begins as the valve store is depressed during actuation. The action of depressing the valve strap campes the formation of a transient metaring chamber, which is in this communication with the residual metering volume defined by the next) amount gap. As the valve term is depressed, the transient portion of the metering chamber expends and flameholder extents the metaring chamber. As displacement of the valve pers continues, a stage is reached at which filling of the trendent metering chamber stops.

Eventually, dispherement of the valve stem continues to the discharge stage, in which the metered formulation is discharged. In these valves, a simple actuation thus causes rapid filling of the transient metaring chamber followed by discharge of the

2

foundation to the patient. Generally, metrard flammlation does not reside the any approximate length of time in the metraing chamber in these metraing valves. However, some flammlation may reside in the residual metraing volume defined by the small annular gap when the metraing valve is at rest.

Some metaring valves limit the beight of the annals: gap, thereby reducing the regional volume and limiting the amount of framulation that resides in the metaring chamber between activation events.

While a metering valve having a transient metaling chamber provides advantages over other types of metering valves for the delivery of across formulations, the flow of formulation from the comminer to the metering chamber may be disrupted. Disrupted flow of formulation refers to filling a metering chamber through one or more botherock regions of significantly restricted access. Flow through the botherock regions may be impeded sufficiently to give size to substantially incomplete filling of the metering chamber, particularly under conditions typical of patient use. When this happens, formulation may be delivered in incommittent or inaccurate doses. Of course, all metering chamber iniets become significantly restricted immediately prior to being scaled off during actuation. Disrupted flow, as just described, refers to flow access during the majority of the filling stress of actuation.

Centain metoring valves have been designed to improve the flow of formulation into the metering channels. For example, some metering valves include angled spillway filling channels designed to limit disruption of the flow of formulation into the metering channels. Less disrupted flow may decrease the likelihood and extent to which vapor or air voids from in the meteriod volume and, therefore improve performance of the metering valve.

Summary of the Invention

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The present invention relates to a povel design for a metering valve that provides improved consistency of formulation delivery. The metering valve of the present invention includes a valve stem designed to (1) limit or eliminate the residual metering volume, thereby reducing the amount of formulation that resides in the metering chamber while the metering valve is at rest, and (2) limit restrictions on the free flow of formulation

WO 2004/022142 PCT/US2003/027587

FIG. 11 is an embraced cross-sectional view of an alternative embodiment of a valve stem according to the present invention.

FIG. 12 is an embrged cross-sectional view of another alternative embodiment of a valve stem according to the present invention.

Detailed Description of the Invention

The following description is set forth in terms of an seroes) metering valve used to dispense an seroes) formulation from an seroes) container. However, the metering valve and methods of the present invention have application to virtually any prosturized fluid requiring delivery of an accurate, meternel dose. In particular, the metering valves described hereis are useful for dispensing medicinal seroes) formulations.

When used to dispense medicinal serosol framinisms, a matering valve according to the present invention may be used to administer virtually any serosol framulation of drug into a body cavity of a patient, such as the month, nose, axes, vagina, cara, or onto the eyes or any skin area of the patient. However, the present invention is not limited to medicinal applications and may be used whenever a parties amount of material from a pressurined fluid is to be delivered to a given region.

FIG. 1 shows so sensed dispensing appearins, generally designated as 10, that incorporates one embodiment of a metering valve 14 according to the present invention. The top end of the metering valve 14 is crimped amound the end of a conventional sensed container 12, while a conventional discharge piece 16 is mounted around the bottom of the metering valve 14. Thus, sensed formulation is dispensed downwardly from the according to the metering valve 14, then through the discharge piece 16 where it is delivered to a patient. The discharge piece 16 directs the according toward the body cavity or other area to which the formulation is to be delivered. For example, discharge piece 16 may be a mornholess that can be inserted into the patient's mouth, thereby providing onal administration of the across formulation.

The account-dispensing device shows in FIG. I is merely one example of how a metaling valve according to the present invention can be incorporated into a dispensing appearant. Furthermore, the configuration of the discharge pieces 16 depends upon the application for the acrossl.

WO 1044012142 PCT/IIS1943/027587

into the matering chamber. Consequently, consistent delivery of framulation is obtained by reducing the effects of loss of prime and loss of door.

The present invention provides an aerosol metering valve that includes a valvo stem that generally defines a longitudinal axis, a valve body, and a inetering gasket configured to be abin to form a transient, substantially fluid-tight thes seal between the valve stem and a scaling portion of the valve body. The valve stem includes a body portion including a proximal end, a distal end, and at least one side surface connecting the proximal end and the distal end and including a metaring surface, wherein the longitudinal axis and a plane tangential to at least a portion of the matering nurface define an angle from about 2° to about 90°.

Brief Description of the Denwines

FIG. 1 is a cross-sectional view of a meterod dose inhaler including an embodiment of the acrossol metering valve according to the present invention.

FIG. 2 is an enlarged cross-sectional view of one embodiment of another acrosol.

metering valve according to the present invention in the resting position.

FIG. 3 is an enlarged cross-sectional view of the sensed metering valve shown in FIG. 2 during the filling stage of valve etem actuation.

FIG. 4 is an enlarged cross-sectional view of the serosol metering valve shown in FIG. 2 at the filled stage of valve stem semation.

FIG. 5 is an enlarged cross-acctional view of the across metering valve shows in FIG. 2 during the discharge stage of valve stem actuation.

FIGS. 6 and 7 are enlarged cross-sectional views of the embodiment of an acrossimetering valve shown in Figure 1 in the resting position and during the discharge stage of the valve stem actuation, respectively.

FIGS. 8 and 9 are enlarged cross-sectional views of a further embodiment of an acrosol metering valve according to the present invention in the resting position and during the discharge stage of the valve stem according.

FIG. 10 is an enlarged cross-exchanal view of one embodiment of a valve stam

according to the present invention.

WO 2004/022142 PCT/US2003/027587

In many of the figures, a metering valve or valve atom is shown in isolation for case of illustration. The valve stems shown in isolation may be combined with one or more additional components to form a metering valve. Such metering valves, as well as metering valves shown in isolation in the figures, may be combined with one or more additional components to form an acrosol dispensing device. It is understood that any particular feature shown in a metering valve and/or valve atom embodiment may be combined with framers shown in other embodiments and/or incorporated appropriately within other embodiments.

Referring to FIG. 2 showing an embodiment of a metering valve 14 (in the resting position), the metering valve 14 typically includes a housing 18 that serves to house the various components of the metering valve 14. The top portion of the housing 18 anaches to the acrosol container 12 (as exemplarily shown in FIG.1). A valve body 21, typically sexted within the valve housing 18, in turn provides a housing for a valve stem 26. The valve body 22 includes an interior surface 24 defining an internal chamber or cavity of the valve body.

The metering valve 14 typically includes a spring cago 46 that, together with the valve body 22, defines an interior chamber 32, a portion of which is occupied by a portion of the valve stem 26. One or more inlets (not shown) typically traversing the spring cago provide open and unrestricted fluid communication between the interior chamber 32 and the access) container 12.

The valve stem 26 includes two partiess, a body parties and a stem parties. The stem portion includes that parties of the valve stem that is conside the valve bouring 18 when the valve stem 26 is in the resting position shows in FIG. 2. During actuation of the valve stem 26, however, the stem portion will be displaced inwardly with respect to the metaning valve 14, as described mean fully below, so that some of the stem portion will be transiently positioned inside the valve bouring 13. The stem portion includes a passageway 50 through which a metered dose of the installation is discharged, as will be described more fully below. The passageway includes one or more side bales 52.

The body portion of the valve stars 26 is that portion that is positioned within the valve bouning 18 theorethout extraction of the valve stars 26. The body portion of the valve stars 26 (as shown in FRGS, 2-5) includes a meaning embors 28 and a scaling surface 30.

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The body parties of the valve stem 26 is configured to have substantially the same that as the remounting wall of the valve body 22. Thus, as can be seen in the embediment shows in FIG. 2, a substantial portion of the matering surface 22 of valve stem 26 rests in counset with the interior surface of the valve body 24 when the metering valve is in the resting position, thereby minimizing, if not eliminating, the samelar gap between the valve stem and valve body when the metering valve is in the resting position, and thus minimizing, if not eliminating, if not eliminating residual metering volume.

The metering valve may include a spring guide 44 mounted on the end of the valve stem body portion opposite the stem portion and a spring 48 within the interior chamber 38 of the metering valve as shown in FIG. 2. The spring 48 through engagement with the spring guide biases the valve stem 26 toward the resting position. It will be appreciated by those shilled in the set that any suitable means for biasing the valve stem 26 into the resting position, e.g. coil compression spring or a spring appropriately mounted external to the interior chamber, may be used in connection with metering valves according to the present invention. The spring guide may be an integral part of the valve stem and/or arranged to include a pressure filling ring as described in the US Patent US 5,400,920, which is incorporated by reference berein.

The metering valve 14 also includes at least two annular gashets, the displacem 20 and the metering gashet 32. The displacem 20 is positioned between the valve housing 18, the valve body 12 and the valve stem 26, as shown in FIG. 2. The displacem 20 isolates the formulation in the acrosol container 12 from the extenior of the valve by forming two fluid tight scale: 1) an annular sliding scal between the displacem 20 and the valve stem 26 where the valve stem extends out of the valve housing, and 2) two compressive planer or face scale between the valve body 22, the displacem 20 and the housing 18. The latter scal may be effected either with or without a scaling bead on either the valve body 22 or the housing 18.

In the embediment shown in FIGS. 2-5, the metering gasket 32 is included in the body wall of the valve body, being generally positioned between the valve body 22, the spring cage 46, and the body portion of the valve stem 26. The metering gasket 32 forms two finid right compressive planer or face scale between the metering gasket 32 and the

9/O 2004/822142 PCT/US2003/827587

chamber 38, the formulation passes between the spring guide 44 and the metraing guide 32. Formulation flows eround the preximal end of the valve stem 26 between the valve stem 26 and the interior surface of the valve body 24 and enters the expanding metraing chamber 34. The spring guide may be provided with cut-away portions or openings to improve flow and/or access to the metraing chamber.

Thus, as the valve stem 26 is moved from the resting position shown in FIG. 2 to the filling stage shown in FIG. 3, served firmulation passes from the acrossol container 12 to the metering chember 34 immediately upon actuation of the valve stem 26. Formulation continues to fill the metering chember 34 until the metering valve 14 reaches the filled stage as depicted in FIG. 4. As will be described in more detail below, the flow of firmulation into the metering chember 34 may be affected by the angle described by the metering arrives of the valve stem 28 with respect to the central longitudinal axis of the makes over

At the end of the filling etters, the flow path of formulation from the acrosol container 12 to the metering chamber 34 is cut off as the metering garket 32 contacts the scaling surface 30 of the valve stem 26, as can be seen in FIG. 4. The metering garket 32 forms a fluid-cight, face seal with the scaling surface 30, thereby concluding filling of the metering chamber 34 and isolating the metering chamber prior to discharge. The scaling surface 30 may be provided with a scaling bead and may be any shape embable for providing desired scaling characteristics. However, for enhanced scaling performance and valve operation, as discussed in more detail below, the scaling surface 30 is desirably grantally conical and more performancy in its longitudinal cross-section the sides may be either substantially straight-edged (as shown in e.g. FIGA) or concave (as shown in e.g. FIGA).

At this steps, the meterned does of formulation is isolated and mady for discharge from the metering chamber 34 and delivery to the patient. The dimensions of the valve body 23, valve stem 26 and other valve components determine the Elled-volume of the metering chamber 34 in the completely filled position.

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FIG. 5 depicts the messering valve 14 in the discharge stage of actuation. In order to discharge the messed does of accused formulation from the mesself chamber 34, the valve atom 26 is fastist accused to the position illustrated in FIG. 5. Those defined in the

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valve body 22 and the spring cage 46. These may be achieved either with or without a scaling head on the valve body 22 and/or the spring cage 46.

The metering grades in this embodiment or other embodiments in accordance with the present invention may be either mechanically effixed, molded onto the empercise component of the metering valve, or the respective components may be ensemblemed using, for example, a two that or co-molding process in which the corresponding component of the metering valve and metering grades are co-molded to that a strong bond (mechanical and/or chemical) can be achieved between the components.

As shown in FIG. 4, the metering grades 32 transiently isolates the formulation in the exercing chamber 34 from the secreed container 12 by forming a fluid-tight face seal between the metering grades 32 and the scaling surface 30 of the valve atom 26. The metering grades 32 provides a means for terminating the flow of formulation from the second container 12 to the metering chamber 34 during actuation of the valve stem 26, as will be described in more detail below.

Operation of the metering valve 14 shown in FIG. 2 is illustrated in FIGS. 3, 4 and 5. The figures illustrate the stages of operation of the metering valve 14 and the corresponding relative positions of the valve components so a patient actuates the valve stem 26, thereby releasing a dose of acrosol formulation. FIG. 3 shows the metering valve 14 in the filling stage, FIG. 4 shows the metering valve 14 in the filled stage, and FIG. 5 shows the metering valve 14 in the filled stage.

As can be seen in FIG. 3 during the filling stage of actuation, the valve stem 26 has been displaced inwardly into the interior chamber 38 against the compressive force of the spring 48. As the valve stem 26 is displaced inwardly, the proximal end of the stem portion of the valve stem 26 enters the valve bouring 18. As a result, a metering chamber 34 is formed between the interior surface of the valve body 24 and the metering surface 28 of the valve stem 26. The volume of the metering chamber 34 increases as the valve stem is displaced until it matches its filled-volume at the cod of the filling stage as depicted in FIG. 4 showing the completely filled position.

Acrosol formulation enters the filling volume of the metering chamber 34 in the following manner. Formulation from the acrosol container 12 passes through the one or more injects and into the interior chamber 38 of the metering valve. From the interior

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art will realize that the distance traveled by the valve stem 26 between PIG, 4 and FIG. 5 will result in an expansion of the metering chamber 34 without increasing the metered does. The extra travel ensures that the metering grates 33 is scaled against the scaling surface 30 between the one or more side holes 52 enter the metering chamber 34. As can be appreciated from FiGS, 4 and 5, as the valve stem is further actuated from the completely filled-position (as shown in FiG. 4) to the discharge position (allustrated in FiG. 5), the metering grates 32 stretches and the facing contact surfaces of the metering gratest and the scaling surface 30 show a relative movement to one another in reciprocation of the travel of the valve stem. Thus the face scal here may be considered a dynamic, reciprocating face scal. As the valve stem 16 is fully actuated, the one or more side holes 52 of the discharge pastagraway 50 pasts through the dispharges 20 and come into fluid communication with the metering chamber 34. The fluid communication thus established allows the acrossite formulation within the metizing chamber 34 to be released into the one or more side holes 52 and the formulation thus passes through the discharge pastagraway 50, thereby delivering the metered does of scansel formulation to the patient or other desired area.

During the discharge of the across formulation from the metering chamber 34 as shown in FIG. 5, the metering grades 32 continues to proven the passage of additional bulk formulation from the across comminer 12 to the metering chamber 34, with allowance made for the dimensional tolerances of the valve components. After the does of across formulation is discharged, the patient releases the valve stars 26, which returns to its original cesting position depicted in FIG. 2 by at least the bissing action of the spring 48. In some embodiments, the matering grades 32 also may provide bissing action that promotes comm of the valve stars 26 to the resting position.

The executive stepri of valve stem extension, as exemplatily depicted in FIGS. 3, 4 and 3, are all accomplished during the brief duration of actuation of the valve stem.

Accordingly, formation, filling and emptying of the meaning chamber occurs rapidly. At most, only a very small percentage of a dose of formulation staides in the metating chamber between actuations. In some embodiments, the metating chamber cary not exist at all in the tenting state - the testimal metating volume may be zero - so that so formulation can reside in the metating chamber between actuations. Because the stages of valve stran actuation occur rapidly, the metating chamber is full of formulation only the a

brief moment immediately prior to discharge of the formulation from the metaring chamber.

FEGS. 6 and 7 illustrate smother embodiment of a metering valve 14 in its resting position and during discharge stage of extraction. This embodiment provides an example in which the spring guide 44 is formed of two parts, a spring guide atom 44° and a spring guide cap 44°, wherein the valve stem 26 and spring guide atom are formed as a single element and the spring guide cap is formed as a separate element, which is subsequently affixed canb the spring guide stem.

In comparison to the embodiment of FIGS. 2-5, in this embodiment the body portion of the valve sum 25 is configured such that the angle described by a major portion of the metering surface 28 of the valve sum with respect to the central longitudinal satis of the valve stem is larger. During actuation of the metering valve 14, the operation of which is the same as that described for the embodiment illustrated in FIGS. 2-5, free flow of formulation during the filling stage into the metering chamber 34 flamed upon actuation is further enhanced, as discussed in more detail below, due to the declarable configuration of the metering surface 28 of the body portion of the valve stem 26. The scaling surface 39 in this embodiment, similar to the scaling surface in the embodiment depicted in FIGS. 2-5, is also generally conical. This embodiment provides an example of a metering valve including a scaling surface 30, which is substantially concave in its longitudinal cross-section. As can be apprecisted from FIG. 7, this configuration of the scaling surface 30 advantageously facilitates the scaling performance of metering gastiest 32 against the scaling nurface.

FIGS. 8 and 9 (Ibustrate a further embodiment of a metering valve 14 in its resting position and during discharge stage of actuation. This embodiment is similar to the embodiment shown in FIGS. 6 and 7. Here the body portion of the valve stam 26 is configured such that the angle described by a major portion of the metering surface 28 of the valve stam with respect to the contral longitudinal axis of the valve stam is even greater, being about 90°, and the scaling surface 30 is generally conical with substantially straight-edged sides in its longitudinal cross-section.

The configurations of the valve body 22, valve stem 26 and in some cases other valve components influence free flow of formulation and the presence of residual metering

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volume when the metering valve is in its resting position as well as the flow of framulation into the metering chamber 34 when the valve stem is actuated.

For example, when the metering portion (a portion that, in part, bounds the metering chamber formed upon actination) of the valve body is configured to substantially combine to the metering surface of the valve stem, when the metering valve is in its resting position, the presence of residual metering volume is minimized. Under the term "metering portion of the valve body is configured to substantially confirm to the metering surface of the valve stom", it is desirably understood that a significant portion (a.g. \geq 90 %) of the metaring surface of the valve stem sests in courses with the interior surface of the valve body when the metering valve is in the resting position. The residual metering volume may be further minimized, by configuring the metering portion of the valve body to essentially confirm or to confirm to the metering surface of the valve stem when the valve is at sest. Under the term "metering portion of the valve body is configured to essentially conform or to conform to the metering surface of the valve stem", it is desirably understood that substantially the complete portion (e.g. > 95 %) or essentially the complete portion (e.g. ≥ 97.5 % or more desirably ≥ 99 %), respectively, of the metering surface of the valve stem rests in contact with the interior surface of the valve body when the metering valve is in the resting position.

Free flow of formulation in the valve in its rest position may be further desirably influenced, by configuring the metaring surface of the body portion of the valve stam, such that no significant portion (e.g. \leq 5 % or more desirably \leq 2.5 %), more suitably no enterioral portion (e.g. \leq 2 % or more desirably \leq 1 %), or most suitably no portion of the metaring surface adjacent to the interface between the metaring surface and the scaling surface of the body portion of the valve body is aligned parallel or nearly parallel to the stam axis (i.e., with a very small angle 0, e.g., 0' or 1"). Also, free-flowing communication between the bulk formulation and formulation within the interior chamber, in particular in the vicinity of the body portion of the valve stam and the internal chamber or cavity of the valve body defined by the interior surface of the valve body wall, when the metering valve is in the resting position may be enhanced by certain configurations of the scaling surface of the body portion of the valve stam, in particular, it may be desirable to configure the scaling surface of the body portion of the valve stam, and that no significant portion (e.g.

13

WO 2004/022142 PCT/US2043/027587

5.5% or more desirably $\le 2.5\%$), more suitably no substantial portion (e.g. $\le 2\%$ or more desirably $\le 1\%$), or most suitably no parties of the scaling surface adjacent to the intention between the metaring surface and the scaling surface of the body portion of the valve body is aligned parallel or nearly parallel to the stem sais.

As mentioned above, the flow of formulation into the metering chamber during actuation may be affected by the engle described by the metering surface of the valve stem with respect to the central longitudinal axis of the valve stem. For example, the valve stem 24 may define a central longitudinal axis 60, as shown in FIG. 10. An angle 8, may be defined by the intersection of a plane 62 temperatial to a major postion of the matering surface 28 of the valve stem and the central axis 60. In some embodiments with complex prometries, angle 8, may be defined by the intersection of the central axis 60 and a plane temperatial with a minor portion of the metering surface 28, as shown in FIG. 12.

All clue being equal and assuming that the valve body is configured to substantially confirm to the valve stem, a larger θ_n results in a wider filling gap for a given displacement of the valve stem during actuation of the metering valve. For given scaling dismeters and a given stem displacement distance to the metering point, a larger value of θ_n generally allows the valve stem and the metering valve to be shorter. The shape of the metering surface 28 shown in FIG. 12 allows the use of a particular angle θ_n in a shorter metering walve. A simpler metering surface, such as that shows in FIG. 10, may require less dimensional control is order to manufacture the valve stem and valve body that substantially combon to one senther and thereby limit or eliminate residual metering volume when the metering valve is at rest.

Suitable values for engle 0, in valve stems according to the present invention are from about 2° to about 90°. Within this range a minimum angle of about 10° is more desirable, about 20° even more destrable and about 30° must desirable. A maximum angle of about 50° is more desirable, about 70° even more desirable and about 60° most desirable.

To limit the potential of areas of matricard flow within the metering chamber and then enhanced then flow of florardation into the metering chamber, the metering surface is desirably configured to comprise no significant portion (s.g. $\leq 5\%$ or more desirably

WO 2014/022142 PCT/US2003/027587

 \le 2.5 %), more suitably no substantial portion (e.g. \le 2 % or more desirably \le 1 %), or most suitably no portion stigned penallel or nearly parallel to the stem exis.

As can be seen in the exemplary embediments shown in FIGS. 2, 6 and 8, the body portion of the valve stem typically includes a section adjacent to the stem portion, which is aligned parallel or manly parallel to the stem axis. This section facilitates the passage of the valve stem through the opening of the valve housing end/or the displacent. Because this section is adjacent to the stem portion and at the distal end of the metering chamber formed upon actuation (as can be appreciated for example in FIG. 3), a parallel or nearly parallel alignment of this section of body portion does not restrict the flow into the metering chamber.

As can be best seen in FEGS. 10 to 12 abowing exemplary valve sums, the mettering surface 28 is typically that surface of the section of the body portion located between the section of the body portion comprising the sealing surface 30 and the section of the body portion edjacent to the stem portion being aligned parallel or occurly parallel to the stem actio. The circumferential interface or boundary of the metering surface and the sealing surface may generally be understood to be the summins of widest transverse cross section of the valve stem body. In embodiments, which in accordance to the afterward definition would have an interface or boundary having a portion parallel to the longitudinal axis of the stem, the interface or boundary is typically understood in this case to be the number at the parallel end of the parallel portion (i.e. the end distant from the stem portion). As can be appreciated from FIGS. 10 to 12, if the valve stem includes a mounted or integral spring guide 44, the sealing surface 30 typically ends at the interface or boundary between the surface of the body portion of the valve stem and the surface of the spring guide.

The scaling characteristics end/or the flow of faraminion into the metering chamber during estantian end/or free flow of faraminion when the metering valve is at rest may also be effected by configuration of the scaling cathon, and as mentioned shows, the scaling surface 30 is desirably generally conical and more particularly in its beginninal errors-section the sides are either substantially straight-edged or conserve. The engle described by the scaling surface of the valve sums with scapect to the control longitudinal axis of the valve sum may also have an effect.

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Referring to FIG. 10, an engle 0, may be defined by the intersection of a plane 64 tangential to a major portion of the scaling nurbace 30 of the valve stem and the central axis 60. Typical values for engle 0, may be from about 30° to about 20°. Within this range, a minimum angle of about 35° is more destrable and about 40° most destrable. A sustinum angle of about 75° is more destrable and about 70° most destrable. In some embodiments, angle 0, may be defined by the intersection of the central axis 60 and a plane tangential with a minur portion of the scaling surface 30. For embodiments in which the scaling nurbace is generally conical in from with concave sides in its longitudinal cross-section, angles of 0, may be defined along the entire concave author by the intersection of the central axis 60 and planes tangential to the curved surface; the values of these angles are desirably all within the sanges defined above.

Menting valves having an angle $\theta_{\rm e}$ in the ranges described may have a metazing postion - a postion that, in part, bounds the metazing chamber - that can generally be described at conical in shape with a cross-sectional area of the proximal portion of the cross-being greater than the cross-sectional area of the distal portion of the cross. In some embodiments, the manaverse cross-sectional area of the valve area body at the metazing and scaling surface interface may be about 4% greater than the transverse cross-sectional area of the distal end (i.e. towards the stem portion of the valve atom) of the valve atom body at the metazing body. In other embodiments, the transverse cross-sectional area of the valve atom body at the metazing and scaling surface interface may be at least about 20% greater than the transverse cross-sectional area of the valve atom body at the metazing embodiments, the transverse cross-sectional area of the valve atom body at the metazing and scaling surface interface may be at least about 60% greater than the transverse cross-sectional area of the distal end of the valve atom body at the metazing and scaling surface interface may be at least about 60% greater than the transverse cross-sectional area of the distal end of the valve atom body.

In certain embodiments having a generally conical metering portion, the interior surface of the valve body maintains a generally conical form from the displangm to the valve body scaling surface.

The metering surface 28 of the valve stem 26 may be of any suitable configuration and still define the plane 62 used to define single 0. For example, in a valve stem having substively simple geometry, such as the valve stem shown in FIG. 10, a majority of the metering surface 28 may define the plane 62 used to define angle 0. Alternatively, the

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WO 2004/R22142 PCT/US2003/027587

of the present invention may be used in conjunction with general metaring valve designs other than those explicitly shown in the Figures. Such alternative metaring valve designs may include one or more additional fixtures of the valve stem, valve body, or any other portion of the metering valve designed to improve performance of the metering valve. Such additional design fixtures may improve metering valve performance by improving performance parameters including but not limited to formulation flow from the acrossis container to the metering chamber during actuation and consistency of formulation metering.

Various modifications and abstractions to this invention will become apparent to those shilled in the set without departing from the scope and spirit of this invention. It should be understood that this invention is not intended to be underly limited by the litherative embediments and examples set that berein and that such examples and embediments are presented by way of example only with the ecops of the invention intended to be limited only by the claims set that beach as follows.

metering surface 28 may be integrated, such as is shown in FIGS. 11 and 12, and only a portion of the metering surface may be used to define the phase 62. Additionally, irregularities in the metering surface 28 may be non-geometrical and still provide a suitable configuration for valve stem 26 according to the present invention.

Thus, the particular geometry of the metering surface 28 is not critical so long as (1) angle 8, can be defined as described herein, (2) the interior surface 24 of the valve body 22 is configured to substantially conform to the geometry of the metering surface 28. These factors contribute to limiting or eliminating residual metering volume when the metering valve is at rest and facilitate the reduction of restriction of the flow of farmulation to the metering clamber. Purthermore, it may be advantageous for limiting or eliminating residual metering volume that no significant portion of the metering surface and/or the scaling surface adjacent to the interface between the metering surface and the scaling surface is aligned parallel or hearly parallel to the stem axis. The metering surface may be configured to have no significant or substantial portion or more desirably, no portion aligned parallel or nearly parallel to the stem axis. This may contribute to limiting the farmation of areas of restricted flow within the metering chamber and thus restriction on the free flow of formulation into the metering chamber even though the interior surface 24 of the valve body 22 substantially conforms to the geometry of the metering armines 28.

Simple geometries for the matering surface 28 and the interior surface 24 of the valve body may provide certain manufacturing advantages. For example, valve stress baving complete 360° rotational symmetry require no rotational alignment during valve essembly. Simple shapes such as cones might also confir certain performance advantages. For example, simple shapes may rotate problems with deposition of drug or with framulation flow discontinuities at angular edges. However, more complex geometries also are equable for valve stress 26 according to the present invention. Per example, some embediments may include hemispherical or other curved configurations. Other embediments may include valve stress baving multiple angles, such as those shown in FRGS. 11 and 12.

The design of the metering surfaces according to the present invention may contribute, along with other aspects of metering valve or valve stem design, to improve the flow of framulation through the metering valve during actuation. Accordingly, the designs

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WO 2004/022142

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PCT/052903/027587

What is Chimed is:

- 1. An acrosol metering valve compaising:
 - (a) a valve stem that generally defines a longitudinal sais and comprises:
 - (1) a body portion comprising a proximal end, a distal end, and at least one side surface commercing the proximal end and the distal end and comprising a metering surface, wherein the longitudinal axis and a plane tangential to at least a position of the metering surface define an angle from about 2° to about 90°, and
 - (2) a stem portion comprising a discharge passageway,
 - (b) a valve body comprising:
 - (1) a body wall that comprises a scaling postion.
 - (2) an internal chamber defined at least in part by the body wall and comprising a metaring portion configured to substantially combine to the metaring surface of the valve stem, and
- (3) a displange baving walls that define an aperture in slidable, scaling engagement with the stem portion of the valve stem; and (c) a metering gaster configured to be able to from a transient, enterentially fluid-tight face seed between the valve stem and the scaling portion of the body wall.
- An acrosol metering valve according to chain 1, wherein the body well scaling
 portion comprises the metering gasket, which is configured to be able to from a transient,
 substantially fluid-tight face seal with at least a portion of the proximal end of the valve
 stem body.
- 3. An accession mentaing valve according to chain 2, wherein the body portion of the valve tion comprises a scaling surface adjacent to the mentaing surface and distant from the stem portion of the valve stem and wherein said scaling surface and the metering surface from a circumferential introflets on the surface of the valve stem body portion.
- 4. An expect matering valve eccenting to claim 3, wherein no significent postion of the matering station entities the scaling station of the valve than edjected to the interface.

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WO 2004/22142 PCT/US2003/027587

between the metering surface and the scaling arribos is aligned parallel or nearly parallel to the longitudinal axis.

- An account metering valve according to claim 3 or 4, wherein the scaling nurthers is
 generally conical or conical.
 - 6. An ecrossi metering valve according to claim 5, wherein the sides of the scaling surface in its longitudinal cross-section are substantially straight-edged or straight-edged.
- 10 7. An accord metering valve according to claim 5, wherein the sides of the scaling nurses in its longitudinal cross-section are substantially concave or concave.
- 8. An acrosol metering valve according to any of claims 3 to 7, wherein the longitudinal axis and a plane tragential to at least a portion of the scaling surface dufine at 15 angle from about 30° to about 80°.
 - 9. An acrossi metering valve according to any preceding claim, wherein the metering surface is generally conical or conical.
- 20 10. An ecosed metering valve according to any preceding chaim, wherein the angle of the metaring surface is equal to or greater than about 10°.

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- 11. An across) metering valve according to any preceding civin, wherein said engle of metering surface is equal to or greater then about 20°.
- 12. An acrossil metering walve according to any proceeding claim, wherein said angle of metering surface is equal to or greater than about 30°.
- An acrosol metering valve according to any preceding of claim, wherein said engial
 of metering surface is equal to or less than about 80°.

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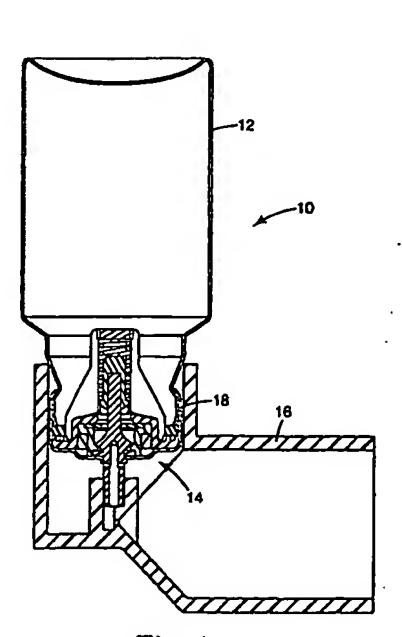


Fig. 1

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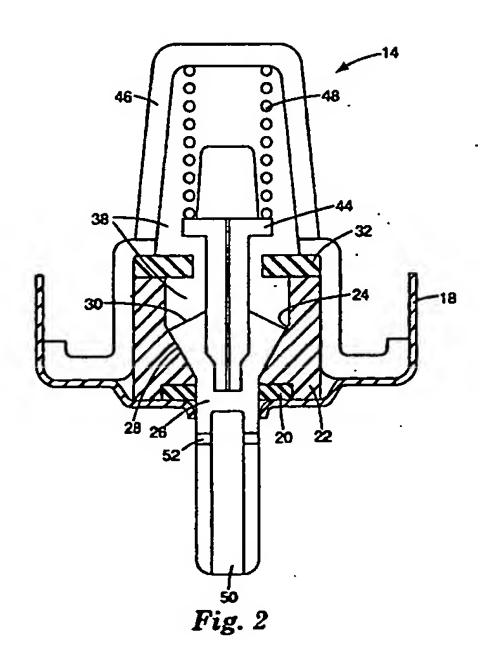
14. An ecrosol metering valve according to any preceding of chain, wherein said angle of mezering surface is equal to or less than about 70°.

- 15. An acrosol metaring valve according to any preceding of claim, wherein said angle of metering surface is equal to or less than about 60°.
 - 16. An acrosol metering valve according to any preceding claim, wherein the metering surface comprises no significant portion aligned parallel or nearly parallel to the longitudinal axis.
 - 17. A meteod doze dispensing device comprising an ecrosed metering valve according to any proceeding claim.
- 18. A metered dose dispensing device according to claim 17, wherein said metered
 dose dispensing device is a metered dose inhaler.

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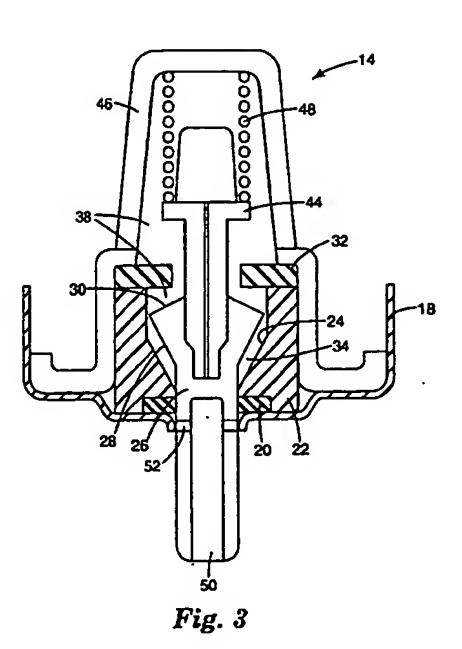
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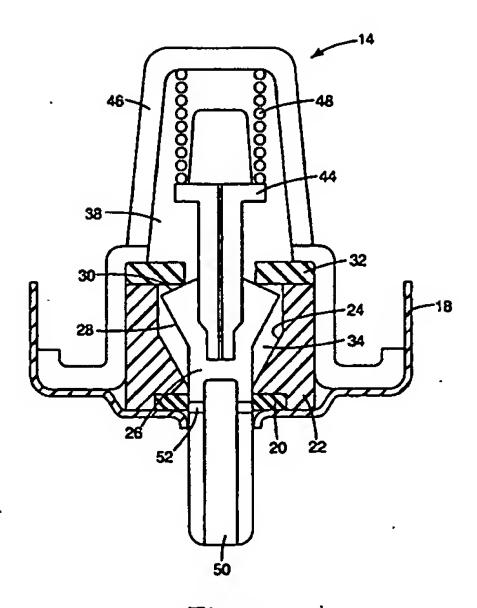
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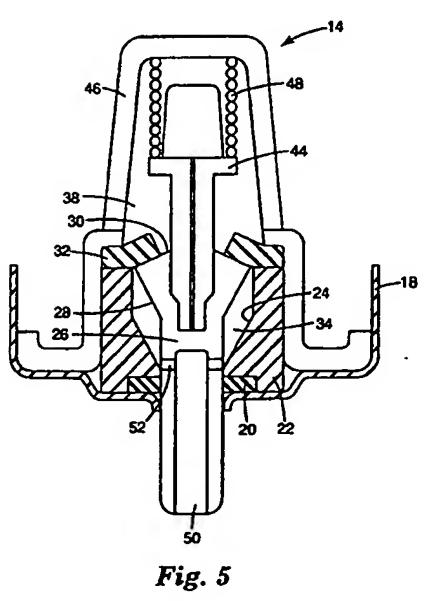
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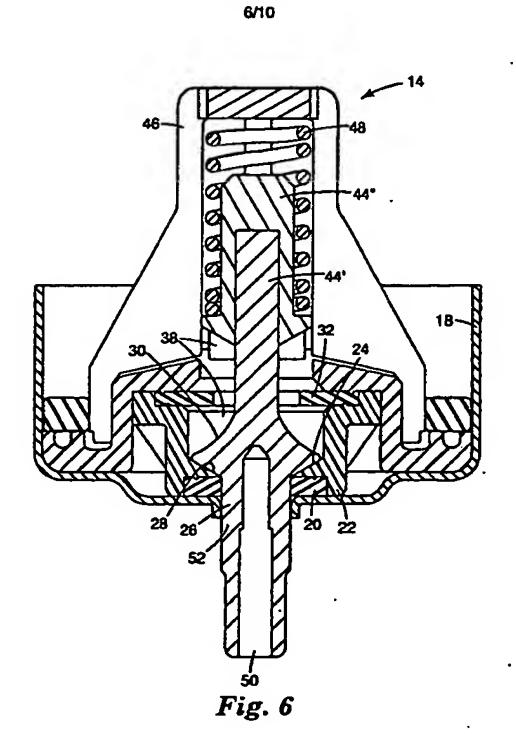
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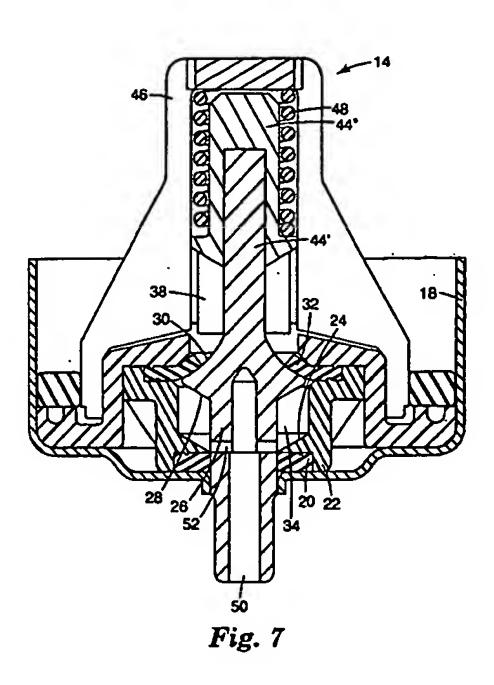
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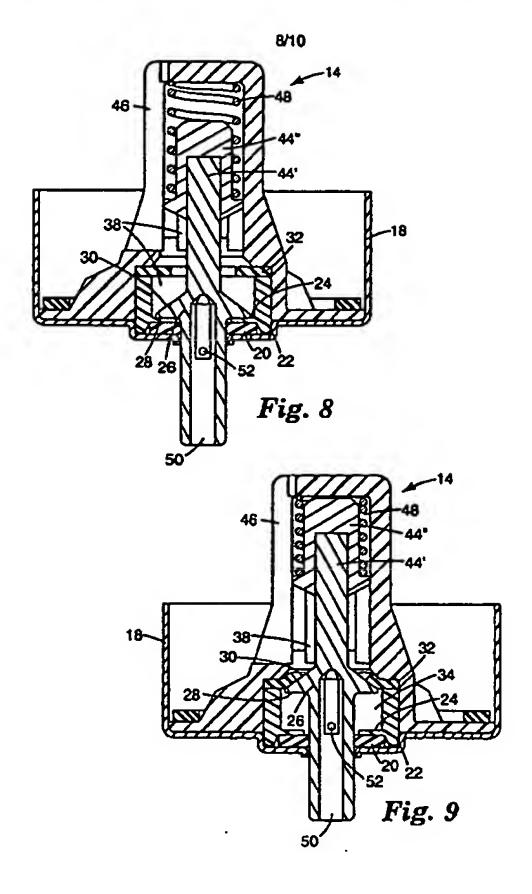
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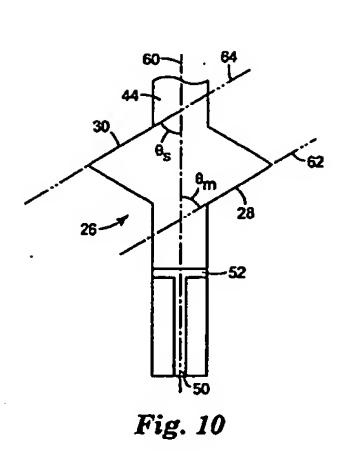


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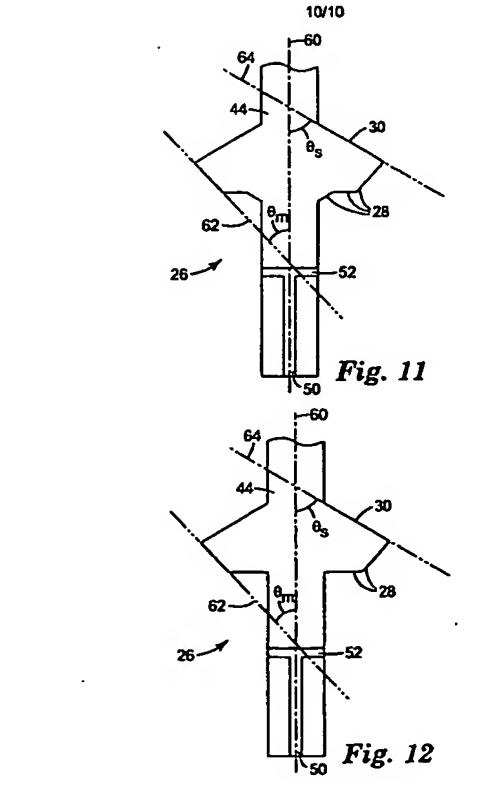
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